



HIT-CT 100 INJECTION MORTAR

Product Technical Datasheet
Concrete-to-concrete
Update: Jun 24



HIT-CT 100 injection mortars

Rebar design (EN 1992-1, EN 1998-1) / Rebar elements / Concrete

Injection mortar system

Benefits



Hilti HIT-CT 100

(330 / 500 ml foil pack)



Rebar ($\phi 8$ - $\phi 25$)

-  technology: Makes installation steps faster, simpler, and safer. Automatic borehole cleaning with hollow drill bits and accurate dosing with HDE.
- Suitable for concrete C12/15 to C50/60.
- Suitable for dry and water saturated concrete.
- For rebar diameters up to 25 mm for static design according to EN 1992-1-1.
- Non-corrosive to rebars.
- Good load capacity at elevated temperatures.
- Suitable for embedment lengths up to 700 mm.
- Suitable for applications down to -5°C concrete temperature.



Application condition

Base material		Load conditions	
Concrete (uncracked)	Concrete (cracked)	Static/ quasi-static	Fire Resistance
Installation conditions		Other information	
Hammer drilled holes	Hollow drill bit drilling	PROFIS Engineering Design Software	Concrete-to- Concrete connections Handbook

Linked Approvals/Certificates

Approval no	Application / loading condition	Authority / Laboratory	Date of issue
ETA-24/0147	Static and quasi-static / Fire	CSTB, Paris	30-04-2024

Linked Instructions for use

Material			
Injection mortar	IFU Hilti HIT-CT 100	-	-
Dispenser	IFU HDM	IFU HDE 500-22	IFU HDE 500-A12

Links/QR codes to Hilti Webpage

Injection mortars / Dispenser			
Hilti HIT-CT 100	HDE 500-22	HDE 500-A12	HDM 500

Mechanical properties and dimensions rebar

Mechanical properties and dimensions of the rebars are standardized and can be taken from the ETA

Material quality

Part	Material
Rebar	Bars and de-coiled rods class B or C according to NDP or NCL of EN 1992-1-1

Static and quasi-static loading based on ETA-24/0147. Design according to EN 1992-1-1

Note the following for the data in this section:

For poor bond conditions multiply the values by 0,7. Values valid for uncracked and cracked concrete.

Design bond strength in N/mm² for good bond conditions for all drilling methods according to mortar IFU.

Rebar - size [mm]	Concrete class								
	C12/15	C16/20	C20/25	C25/30	C30/37	C35/45	C40/50	C45/55	C50/60
$\phi 8 - \phi 25$	$f_{bd,PIR}$ [N/mm ²]								
$\phi 8 - \phi 25$	1,6	2,0	2,3	2,7	3,0	3,0	3,0	3,0	3,0

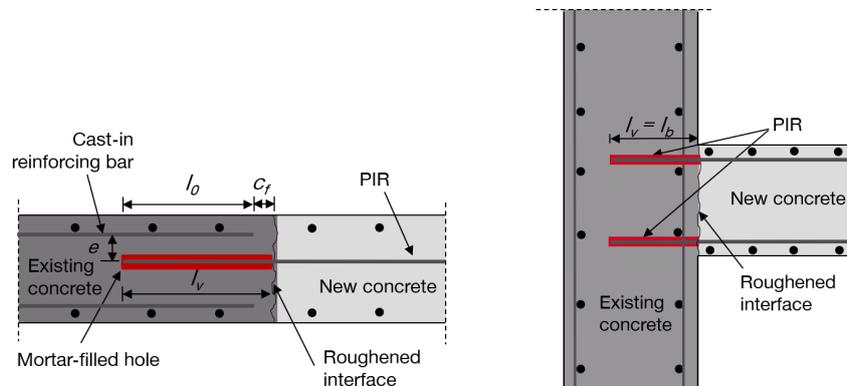
Minimum anchorage length and minimum lap length

Post-installed rebar applications as per EN 1992-1-1	Typical examples
Lap splice applications	
End anchorage applications simply supported / compression load-only connections	

The minimum anchorage length $l_{b,min}$ and the minimum lap length $l_{0,min}$ according for applications designed as per EN 1992-1-1 shall be multiplied by relevant **Amplification factor α_{lb}** in the table below.

Amplification factor α_{lb} for the min. anchorage length and min. lap length for all drilling methods.

Rebar - size [mm]	Concrete class								
	C12/15	C16/20	C20/25	C25/30	C30/37	C35/45	C40/50	C45/55	C50/60
$\phi 8 - \phi 25$	α_{lb} [-]								
$\phi 8 - \phi 25$	1,0		1,2		1,4				



Refer to the table for data on dispensers and corresponding maximum embedment depth $l_{v,max}$ due to mortar installation limitations



Minimum Anchorage length and lap length for characteristic steel strength $f_{yk} = 500 \text{ N/mm}^2$ for good bond conditions

For specific design cases refer to [PROFIS Engineering](#).

Rebar-size [mm]	Concrete class	Design Resistance (Yielding) [kN]	$l_{b,min}^{1)}$ [mm]	$l_{o,min}^{2)}$ [mm]	$l_{bd,y}^{3)}$ ($\alpha_2=1$) [mm]	$l_{bd,y}^{4)}$ ($\alpha_2=0.7$) [mm]	$l_{o,PIR,y}^{5)}$ ($\alpha_2=1$) [mm]	$l_{o,PIR,y}^{6)}$ ($\alpha_2=0.7$) [mm]
$\phi 8$	C20/25	21,9	112	200	375	262	562	394
	C30/37 to C50/60		140	280	291	204	436	305
$\phi 10$	C20/25	34,1	141	211	469	328	703	492
	C30/37 to C50/60		153	280	364	255	545	382
$\phi 12$	C20/25	49,2	169	253	562	394	843	590
	C30/37 to C50/60		183	280	436	305	654	458
$\phi 14$	C20/25	66,9	197	295	656	459	984	689
	C30/37 to C50/60		214	321	509	356	763	534
$\phi 16$	C20/25	87,4	225	337	750	525	1124	787
	C30/37 to C50/60		244	366	582	407	873	611
$\phi 18$	C20/25	110,6	253	380	843	590	1265	886
	C30/37 to C50/60		275	412	654	458	982	687
$\phi 20$	C20/25	136,6	281	422	937	656	1406	984
	C30/37 to C50/60		305	458	727	509	1091	763
$\phi 22$	C20/25	165,3	309	464	1031	722	1546	1082
	C30/37 to C50/60		336	504	800	560	1200	840
$\phi 24$	C20/25	196,7	337	506	1124	787	1687	1181
	C30/37 to C50/60		366	550	873	611	1309	916
$\phi 25$	C20/25	213,4	351	527	1171	820	1757	1230
	C30/37 to C50/60		382	573	909	636	1363	954

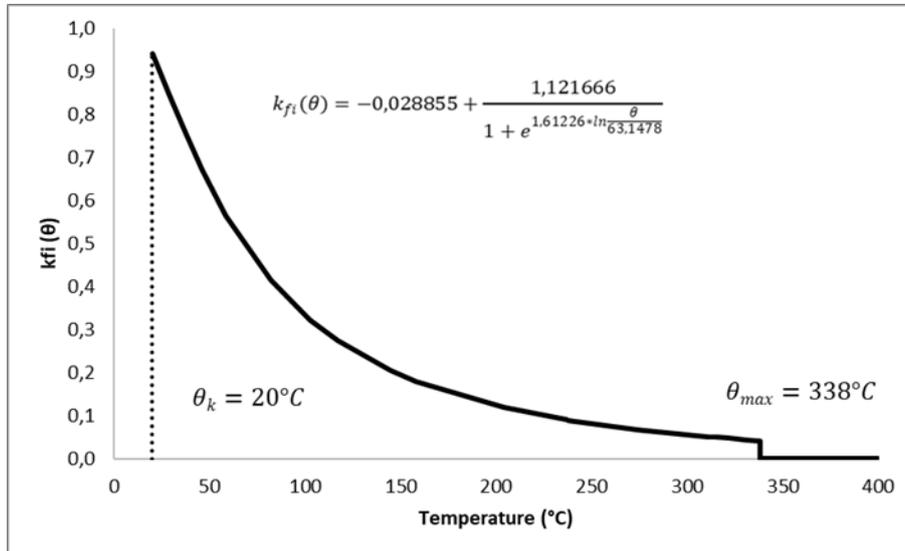
- 1) Minimum anchorage length for simply supported connections under tension loading assuming $\sigma_{sd} = f_{yd}$
- 2) Minimum anchorage length for overlap splice joint for $\alpha_6=1,5$
- 3) Minimum anchorage length for simply supported connections in case of: $\alpha_1= \alpha_2= \alpha_3= \alpha_4= \alpha_5= 1,0$ - (design for yielding)
- 4) Minimum anchorage length for simply supported connections in case of: $\alpha_1= \alpha_3= \alpha_4= \alpha_5= 1$; $\alpha_2= 0,7$ - (design for yielding)
- 5) Minimum anchorage length for overlap joint in case of: $\alpha_1= \alpha_2= \alpha_3= \alpha_4= \alpha_5= 1.0$ - (design for yielding) and $\alpha_6=1,5$
- 6) Minimum anchorage length for overlap joint in case of: $\alpha_1= \alpha_3= \alpha_4= \alpha_5= 1,0$; $\alpha_2= 0.7$ - (design for yielding) and $\alpha_6=1,5$

Fire resistance based on ETA-24/0147 for working life of 50 years

For evidence under fire exposure the anchorage length should be calculated according to EN 1992-1-1:2004+AC:2010 Equation 8.3 using the temperature-dependent bond resistance $f_{bd,fi}$.

For design use [PROFIS Engineering](#).

Temperature reduction factor $k_{fi}(\theta)$ for concrete class C20/25 for good bond conditions



The design value of the bond strength $f_{bd,fi}$ under fire exposure have to be calculated by the following equation:

$$f_{bd,fi} = k_{b,fi}(\theta) \cdot f_{bd,PIR} \cdot \frac{\gamma_c}{\gamma_{M,fi}}$$

With $\theta \leq 338^\circ C$:

$$k_{fi}(\theta) = \frac{f_{bm}(\theta)}{f_{bd,PIR} \cdot 4,3} \leq 1,0$$

Where:

$$f_{bm}(\theta) = -0,28538 + \frac{11,09328}{1 + e^{1,61226 \cdot \ln \frac{\theta}{63,1478}}}$$

$\theta > 338^\circ C$ $k_{fi}(\theta) = 0,0$

- $f_{bd,fi}$ = Design value of the bond resistance in case of fire in N/mm²
- θ = Temperature in °C in the mortar layer
- $k_{b,fi}(\theta)$ = Reduction factor under fire exposure
- $f_{bd,PIR}$ = Design value of the bond resistance in N/mm² in cold condition considering the concrete classes, rebar diameter, the drilling method, and the bond conditions according to EN 1992-1-1
- γ_c = Partial safety factor according to EN 1992-1-1
- $\gamma_{M,fi}$ = Partial safety factor according to EN 1992-1-2

Bond strength $f_{bd,fi}$ in N/mm ² for fire design for concrete classes C20/25 to C50/60						
Rebar Temperature	50°C	100°C	150°C	200°C	250°C	338°C (θ_{max})
$f_{bd,fi}$ [N/mm ²]	2,20	1,15	0,67	0,42	0,28	0,14

Setting information

Installation temperature range

-5°C to +40°C

Service temperature range

Hilti HIT-CT 100 injection mortar may be applied in the temperature ranges given below. An elevated base material temperature may lead to a reduction of the design bond resistance.

Temperature range	Base material temperature	Maximum long-term base material temperature	Maximum short-term base material temperature
Temperature range I	-40 °C to +80 °C	+50 °C	+80 °C

Maximum short term base material temperature

Short-term elevated base material temperatures are those that occur over brief intervals, e.g., as a result of diurnal cycling.

Maximum long term base material temperature

Long-term elevated base material temperatures are roughly constant over significant periods of time.

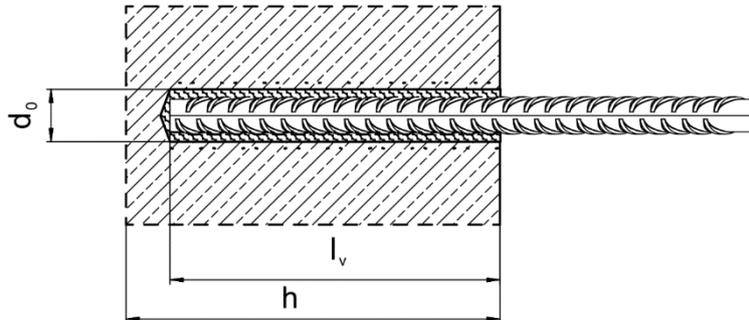
Curing and working time ^{a)}

Temperature of the base material	Maximum working time	Minimum curing time
T	t _{work}	t _{cure} ^{a)}
-5°C to 0°C	30 min	6 h
> 0°C to 5°C	20 min	5 h
> 5°C to 10°C	15 min	4 h
> 10°C to 20°C	8 min	4 h
> 20°C to 30°C	4 min	3,5 h
> 30°C to 40°C	1,5 min	3 h

a) The curing time data are valid for dry base material only. In wet material the curing times must be doubled.

Dispensers and corresponding maximum embedment depth $l_{v,max}$

Rebar	Dispenser	
	HDM 330, HDM 500	HDE 500
	$l_{v,max}$ [mm]	$l_{v,max}$ [mm]
$\phi 8 - \phi 16$	700	700
$\phi 18 - \phi 25$	500	700



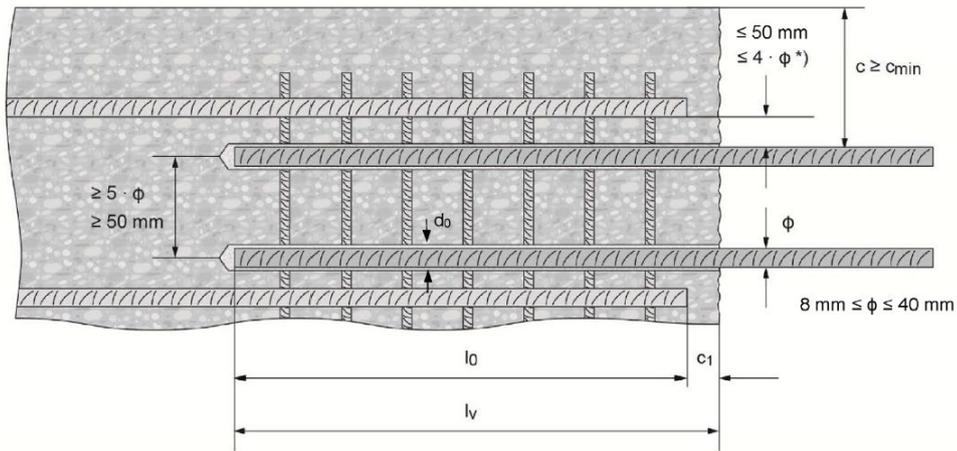
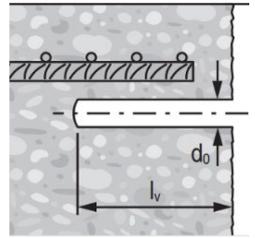
For detailed setting information on installation see instructions for use (IFU) given with the product. Approved installation methods can be found in the specific ETA/Certificate definitions.

Drilling and Installation equipment

Rotary Hammers (Corded and Cordless)		TE 2 - TE 80
Dispenser		HDE HDM
Other tools		Blow out pump, Compressed air gun, Set of cleaning brushes
		Hammer drill bit TE-CX, TE-YX, TE-C, TE-Y
		Hollow drill bit TE-CD, TE-YD
		Piston plug

Minimum concrete cover c_{min} of the post-installed rebar

Drilling method	Bar diameter [mm]	Minimum concrete cover c_{min} [mm]	
		Without drilling aid	With drilling aid
Hammer drilling (HD) and (HDB)	$\phi < 25$	$30 + 0,06 \cdot l_v \geq 2 \cdot \phi$	$30 + 0,02 \cdot l_v \geq 2 \cdot \phi$
	$\phi = 25$	$40 + 0,06 \cdot l_v \geq 2 \cdot \phi$	$40 + 0,02 \cdot l_v \geq 2 \cdot \phi$
Compressed air drilling (CA)	$\phi < 25$	$50 + 0,08 \cdot l_v$	$50 + 0,02 \cdot l_v$
	$\phi = 25$	$60 + 0,08 \cdot l_v \geq 2 \cdot \phi$	$60 + 0,02 \cdot l_v \geq 2 \cdot \phi$



^{*)} If the clear distance between lapped bars exceeds $4 \cdot \phi$ or 50 mm, then the lap length shall be increased by the difference between the clear bar distance and the smaller of $4 \cdot \phi$ or 50 mm.

Where, c is concrete cover of post-installed rebar

$c_1 = c_f$ is the end-cover of existing rebar

d_0 is the nominal drill bit diameter

l_0 is the lap length

l_v is the installation length